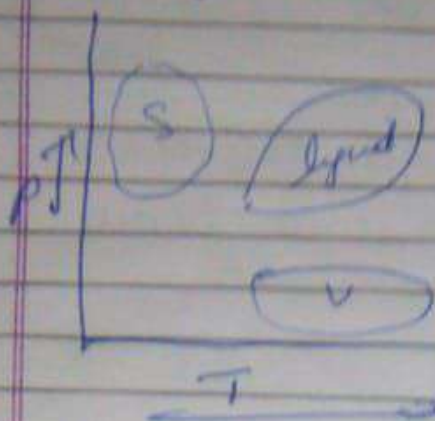


Since to define a one component system is 2, the max degree of freedom is 2, i.e., phase diagram can be drawn in 2 dimensions.



A single phase can be drawn over a region or area since the given phase can exist under different conditions of T & P . i.e. T & P can be varied independently over a range of values without affecting the

existence of single phase.

Solid phase is stable at low T & high P
 Liquid phase is in between these 2 extremes
 Gas phase is at high T & low P

Two phase in equilibrium can be represented by one line, since only one variable is required either T or P has a definite value. If T is stated, the corresponding equilibrium value of P can be determined & vice versa. The no. of lines in a phase diagram will be equal to no. of two phase equilibria which the system can possess.

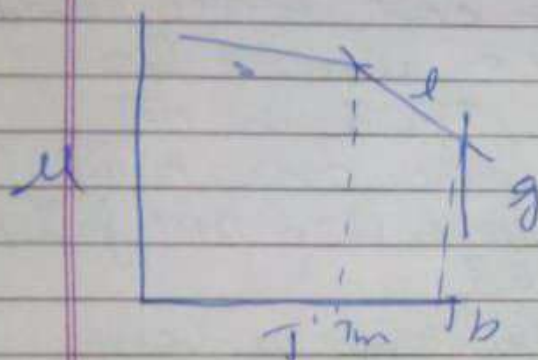
Since for a pure substance $dG = -S_m dT + V_m dP$
 or in terms of chemical potential $d\mu = -S_m dT + V_m dP$
 At const P

$\left(\frac{\partial \mu}{\partial T}\right)_P = -S_m$ The slope of curve drawn between μ and T is equal to $-S_m$.

Since S_m of a given substance in any phase is +ve so slope of the curve $\ln \mu$ vs T should -ve then.

At any temp $S_{m,s} < S_{m,l} < S_{m,g}$
Taking +ve it will reverse the sign
 $-S_{m,s} > -S_{m,l} > -S_{m,g}$

ie the slope of μ vs T curve for a substance has small -ve value since $S_{m,s}$ is small value slope of μ vs T for liquid is slightly more -ve and that for gases is large -ve value



The curve where s & l phase intersect each other at temp T_m . At this temp, chemical potential of substance is same in both solid & liquid phases, $\mu_s = \mu_l$.

Temp T_m is mpt of the solid.

Curves liquid & gaseous phase intersect each at temp T_b where $\mu_l = \mu_g$. It is called boiling point of liquid.

$$d\mu = -S_m dT + v dP$$

At const T , $d\mu = v_m dP = \left(\frac{\partial \mu}{\partial P} \right)_T = v_m$
 $v_{m,g} > v_{m,l} > v_{m,s}$ order of

decreasing chemical potential.

$$(\partial \mu / \partial P)_g > (\partial \mu / \partial P)_l > (\partial \mu / \partial P)_s$$

when pressure of system is reduced. The decrease of chemical with $\downarrow$ of P is maximum for solid phase & largest for gaseous phase eg in the graph, the $\downarrow$ in chemical potential for solid phase is from a to a' , liquid phase b to b' & gases c to c'



The mpt & bpt shifts to lower values as P is decreased, the shift is more for boiling pt. The temp difference betn T_m & T_b $\downarrow$ with $\downarrow$ in P . This shows the temp range over which liquid phase can exist is decreased. If P is decreased to a sufficient low value it may happen liquid is not formed, solid directly passes over to the gaseous phase. This happens when bpt falls below the mpt of solid.

Temp to a sublimating temp is very sensitive to change of P .

When P is $\uparrow$ ed, the effects are exactly opposite. There is $\uparrow$ in mpt & boiling pt of the substance. The $\uparrow$ in bpt is large & enhances the stability of liquid phase. The effect of P on mpt & bpt of substance which shows a $\downarrow$ in volume on melting.

$\downarrow$ of chemical potential of solid will be larger than that of liquid. There occurs $\uparrow$ in mpt as P is $\downarrow$ ed. The $\uparrow$ of P will $\downarrow$ the mpt. eg H₂O, Bi, Sb.

Clapeyron Equation

Let us consider a system in which a pure substance B is present in 2 phases.

α and β . Two phases can be $S \geq L$,
 $L \geq L$ & $S \geq L$

At equilibrium $\mu_B(\alpha) = \mu_B(\beta)$ (1)

Let temp is changed by small amt,
 new equilibrium is established & μ also
 changes by small amount

Chemical pot. can change by small amount

$$\mu_B(\alpha) + d\mu_B(\alpha) = \mu_B(\beta) + d\mu_B(\beta) \quad (2)$$

Sub from (2) eq (2) reduce to

$$d\mu_B(\alpha) = d\mu_B(\beta) \quad (3)$$

$$\alpha \text{ phase: } d\mu_B(\alpha) = -S_{m,B(\alpha)} dT + V_{m,B(\alpha)} dP \quad (4)$$

$$\beta \text{ phase: } d\mu_B(\beta) = -S_{m,B(\beta)} dT + V_{m,B(\beta)} dP \quad (5)$$

Sub. eq (4) in (3)

$$-S_{m,B(\alpha)} dT + V_{m,B(\alpha)} dP = -S_{m,B(\beta)} dT + V_{m,B(\beta)} dP$$

$$S_{m,B(\beta)} \frac{dP}{dT} = + \frac{S_{m,B(\beta)} - S_{m,B(\alpha)}}{V_{m,B(\beta)} - V_{m,B(\alpha)}}$$

$$\frac{dP}{dT} = \frac{\Delta S_{m,\beta}}{\Delta V_{m,\beta}} \quad \begin{array}{l} \text{change in entropy} \\ \text{change in volume} \end{array}$$

This is known as Clapeyron equation

Application of Clapeyron equation $S \rightleftharpoons L$

$$\frac{dP}{dT} = \frac{\Delta S_{fus}}{\Delta V_{m,fus}} = \frac{\Delta H_{fus}}{T \Delta V_{m,fus}}$$

Transformation of solid into liquids is
 an endothermic process & ΔH_{fus} is +ve

ΔV_m can be +ve or -ve depending
 upon which is one is more dense

For most substances $\rho_s > \rho_l$ ΔV_{fus} is +ve but H_2O, Bi, Sb solid phases is less dense than the liquid phase

$$\Delta S_{fus} = 8 \text{ to } 25 \text{ J/K/mole}$$

$$\Delta V_m = 1 \text{ to } 10 \text{ cm}^3 \text{ mole}^{-1}$$

Typical value $\Delta S_{fus} = 20 \text{ J/K/mole}$

$$\Delta V_m = 5 \text{ cm}^3 \text{ mole}^{-1}$$

$$\frac{dp}{dT} = \frac{20 \text{ J/K/mole}}{5 \text{ cm}^3 \text{ mole}^{-1}} = 4 \text{ J/K cm}^3$$

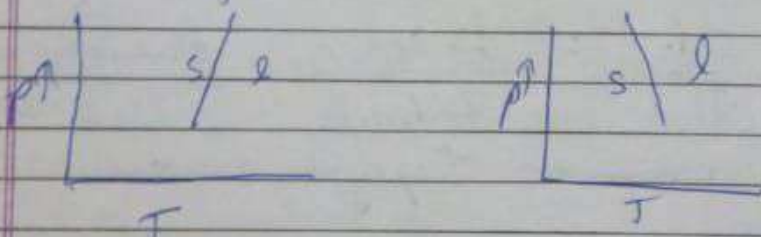
$$= 4 \text{ MPa cm}^3 \text{ K}^{-1} \text{ cm}^{-3}$$

$$= 4 \times 10^3 \text{ K Pa K}^{-1}$$

$$= 4 \times 10^3 \left(\frac{1 \text{ atm}}{101} \right) \text{ K}^{-1}$$

$$= 39.5 \text{ atm K}^{-1}$$

slope of P vs T graph for $S \rightleftharpoons L$ has a large value. Graph is almost vertical. It tilted slightly to left if $\Delta_{fus} V_m$ is -ve



A pt lying anywhere on left of line corresponds to temp below $m.p.T$ of substance & only solid form exist. A pt on right of line corresponds to temp above $m.p.T$, only liquid form exists.

$$\frac{dT}{dP} = \frac{1 \text{ K atm}^{-1}}{39.5} = 0.025 \text{ K atm}^{-1}$$

The change in the mpt of a solid
 Variation of external P is very small
 +ve increase for those substances which show
 an ↑ in volume on mpt whereas -ve
 for a substance where a ↓ in volume
 of on melting is observed

$$\frac{dP}{dT} = \frac{\Delta H_{fus}}{T \Delta V_m T_m}$$

$$P_2 - P_1 = \frac{\Delta H_{fus}}{\Delta V_m T_m} \ln \frac{T_m}{T_m'}$$

$$P_2 - P_1 = \frac{\Delta H_{fus}}{\Delta V_m T_m} \ln \frac{T_m}{T_m'}$$

ΔT is -ve if ΔV_{fus} is +ve

ΔT is -ve if ΔV_{fus} is -ve

$$l \Rightarrow u \quad \Delta H_{fus} = 90 \text{ J/K/mole}$$

$$\Delta V_m = 24 \text{ dm}^3/\text{mole}$$

$$\frac{dP}{dT} = \frac{90 \text{ J/K/mole}}{24 \text{ dm}^3/\text{mole}}$$

$$= 3.75 \text{ kPa/K}$$

$$= 3.75 \text{ kPa/K} \left(\frac{1 \text{ atm}}{101.325 \text{ kPa}} \right) = 0.037 \text{ atm K}^{-1}$$

The value is much smaller
 smaller than s ⇒ l eqn

$$s \Rightarrow l \quad \Delta S_{fus} \text{ sub} = +ve, \Delta V_m = +ve$$

$$\Delta H_{fus} > \Delta H_{vap}$$

$$\left(\frac{dP}{dT} \right)_{s-l} > \left(\frac{dP}{dT} \right)_{l-u}$$