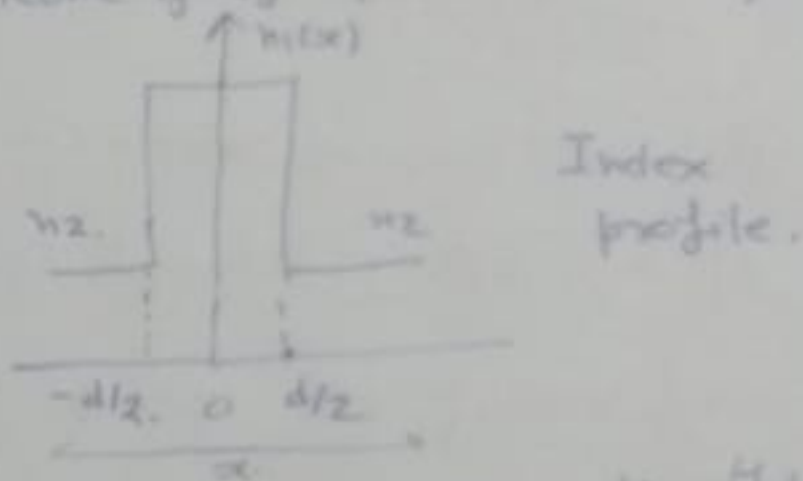
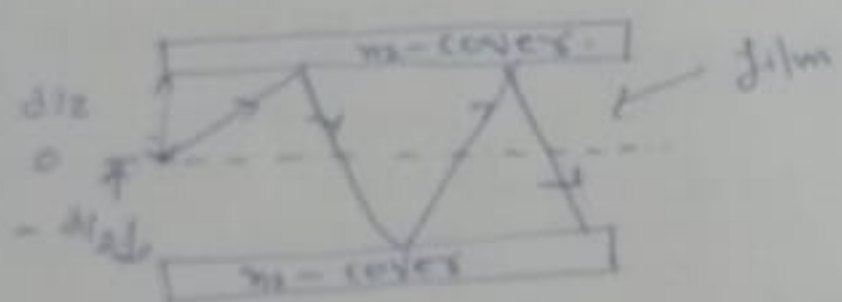
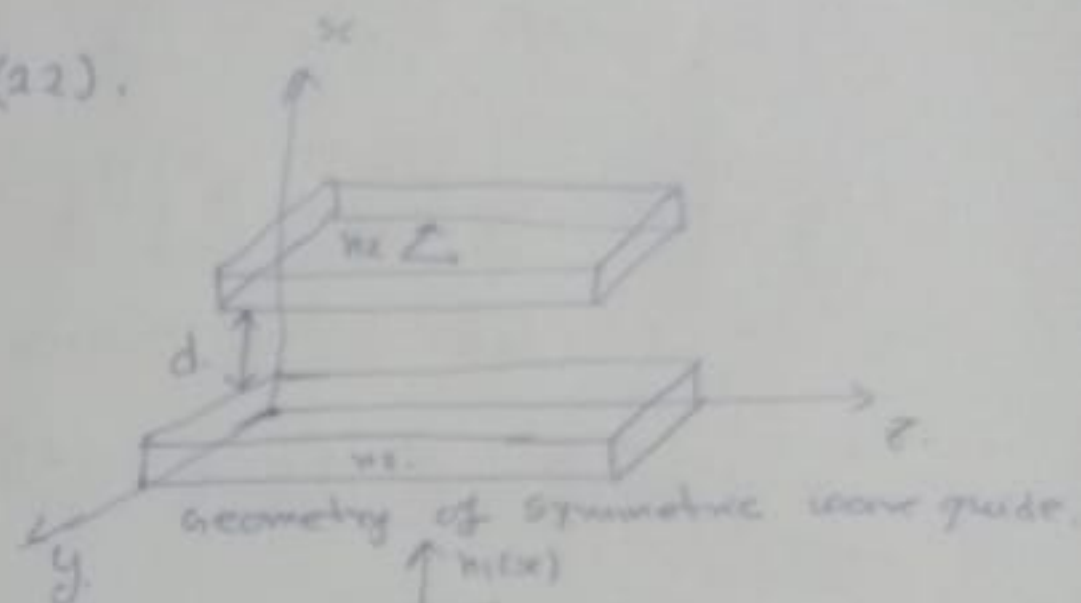
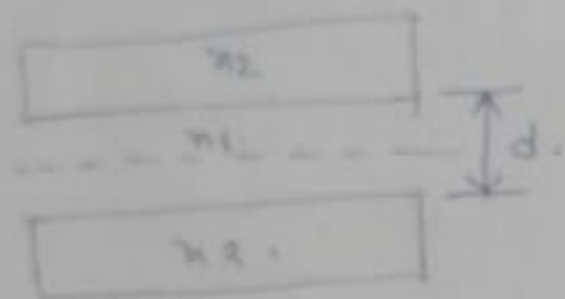


TE modes: Symmetric step Index Planar waveguide.  
 $[E_z = 0]$ .

From part-I,

$$H_{yx} = -\frac{\beta}{\omega \mu_0} E_y \quad \text{eq. (20)}$$

$$H_z = \frac{i}{\omega \mu_0} \frac{\partial E_y}{\partial x} \quad \text{from eq. (22)}$$



$n = n(x)$  is x dependent.

$$n(x) = \begin{cases} n_1 & |x| < d/2 \text{ (film)} \\ n_2 & |x| > d/2 \text{ (cover)} \end{cases} \quad (23)$$

$n_1 > n_2$ . This type of index profile is usually referred to as a step-index profile.

The waveguide is assumed to extend to infinity in y and z directions.

TE mode: Substitute for  $H_x$  (eq. 20) and  $H_z$  (eq. 22) in equation (24), i.e. in

$$-\frac{\partial^2 H_z}{\partial x^2} - i\beta H_x = i\omega \epsilon_0 n^2(x) E_y \quad \text{--- (24)}$$

$$-\frac{\partial^2}{\partial x^2} \left[ \frac{i}{\omega \mu_0} \frac{\partial E_y}{\partial x} \right] - i\beta \left[ -\frac{\beta}{\omega \mu_0} E_y \right] = i\omega \epsilon_0 n^2(x) E_y$$

$$\left[ \frac{\partial}{\partial x} \left( \frac{i}{\omega \mu_0} \frac{\partial E_y}{\partial x} \right) \right] + i\beta \left[ \frac{\beta}{\omega \mu_0} E_y \right] = \omega \epsilon_0 n^2(x) E_y$$

$$\frac{E_y \beta^2}{\omega \mu_0} - \frac{\partial^2 E_y}{\partial x^2} \left( \frac{1}{\omega \mu_0} \right) = \omega \epsilon_0 \tilde{n}(x)^2 E_y$$

$$E_y \beta^2 - \frac{\partial^2 E_y}{\partial x^2} = \omega^2 \mu_0 \epsilon_0 \tilde{n}(x)^2 E_y$$

$$\frac{d^2 E_y}{dx^2} + \omega^2 \mu_0 \epsilon_0 \tilde{n}(x)^2 E_y - \frac{\beta^2}{\omega \mu_0} E_y = 0$$

$$\frac{d^2 E_y}{dx^2} + \left[ \omega^2 \mu_0 \epsilon_0 \tilde{n}(x)^2 - \beta^2 \right] E_y = 0 \quad \text{--- (25)}$$

$$\text{Let } k_0^2 = \omega^2 \mu_0 \epsilon_0 \quad k = \omega \sqrt{\mu_0 \epsilon_0} = k_0 = \frac{\omega}{c} \quad \text{--- (26)}$$

$$\frac{d^2 E_y}{dx^2} + \left[ k_0^2 \tilde{n}(x)^2 - \beta^2 \right] E_y = 0 \quad \text{--- (27)}$$

where,  $\mu_0 \epsilon_0 = \frac{1}{c^2}$  is speed of light in free space.

For the given refractive index profile  $n = \tilde{n}(x)$  solution of eq. (27) [subject to the appropriate B.C. and continuity conditions] will give the field equations corresponding to TE<sub>z</sub> modes of waveguide.

Since  $E_y(x)$  is a tangential component, it should be continuous at any discontinuity, further  $\frac{dE_y}{dx} \propto H_z(x)$  (which is tangential component), it should be continuous at any discontinuity. even

once  $E_y(x)$  is known,  $H_x(x)$  and  $H_z(x)$  can be determined from eq. (18) / eq. (20) eq. (22).

$$n(x) = n_1, \text{ for } x < \left(\frac{d}{2}\right) \text{ in film --- (28)}$$

$$n(x) = n_2 \text{ for } x > \left(\frac{d}{2}\right) \text{ in cover --- 29}$$

Substituting for  $n(x)$  in eq. (28), and (29) in (27)



$$\frac{d^2 E_y}{dx^2} + [k_0^2 n_1^2(x) - \beta^2] E_y = 0 \quad (30) \quad |x| < d/2 \text{ in film.}$$

$$\frac{d^2 E_y}{dx^2} + [k_0^2 n_2^2(x) - \beta^2] E_y = 0 \quad (31) \quad |x| > d/2 \text{ in cover.} \quad (31)$$

We will solve (30), (31) using appropriate boundary and continuity conditions.

ie  $E_x$  &  $H_z$  represent the tangential components on the planes  $x = \pm(d/2)$ , and they must be continuous at  $x = \pm d/2$  and since  $H_z$  is proportional to  $\frac{dE_y}{dx}$ , ie we must have.

$E_y$  and  $\frac{dE_y}{dx}$  continuous at  $x = \pm d/2$ .

For guided wave, fields should decay in cover ie  $|x| > d/2$  or we can say that fields mainly confined to films.

This is possible when  $\beta^2 > k_0^2 n_2^2(x)$  — (32)

if  $\beta^2 < k_0^2 n_2^2(x)$  the solutions are oscillatory in region  $|x| > (d/2)$ . ] then the fields corresponds to radiation modes of wave guide. These modes corresponds to rays that undergoes -refraction (further than total internal reflection), at the film cover. so they leak away.

if  $\beta^2 < k_0^2 n_1^2$  then. modes ~~are~~ field exists inside the core.  $|x| < d/2$ .

To guide the modes this condition is

$$n_2^2(x) k_0^2 < \beta^2 < n_1^2(x) k_0^2 \quad (33).$$

using (33), eq. (31) & eq (32) can be rewritten

as:

$$\frac{d^2 E_y}{dx^2} + \alpha^2 E_y = 0 \quad \text{--- } |\alpha| < \frac{d}{2} \text{ film --- (34)}$$

$$\frac{d^2 E_y}{dx^2} - \gamma^2 E_y = 0 \quad \text{--- } |\alpha| > \frac{d}{2} \text{ cover --- (35)}$$

$$\text{where } \alpha^2 = k_0^2 n_1^2 - \beta^2 \quad \text{--- (36)}$$

$$\gamma^2 = \beta^2 - k_0^2 n_2^2 \quad \text{--- (37)}$$

for symmetric refractive index system  
 $n^2(-x) = n^2(x)$

for wave propagation  $\alpha, \gamma$  should be positive.

if from (37)  $\beta^2 > k_0^2 n_2^2$ ,  $\beta < k_0 n_1$  from (36).

In film  $\frac{d^2 E_y}{dx^2} = -\alpha^2 E_y$ . [if  $\alpha$  is -ve, sol. decays, if  $\alpha$  is +ve, sol. is not oscillatory (loss free)]  
 $\frac{d^2 E_y}{dx^2} = \gamma^2 E_y$ , so the condition is (ie for total internal reflection).

$$k_0 n_1 > \beta > k_0 n_2$$

$E_y(-x) = E_y(x)$  - symmetric modes.

$E_y(-x) = -E_y(x)$  - for anti symmetric modes.

For symmetric modes:

Sol of eq. (35) are, and (34) are

$$E_y = C e^{\gamma x} + D e^{-\gamma x} \quad \text{--- (38) --- in cover.}$$

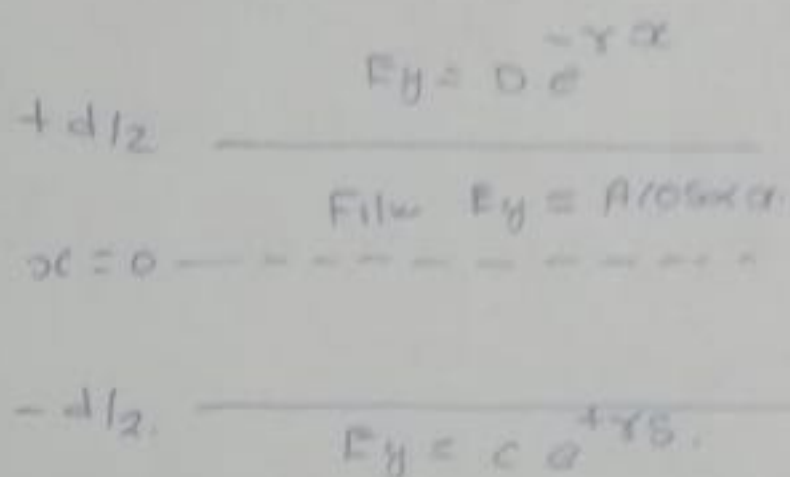
$$E_y = A \cos \alpha x + B \sin \alpha x \quad \text{--- (39) --- in film.}$$

We will neglect the exponentially amplifying solution in the region  $|\alpha| > \frac{d}{2}$

ie for  $x > \frac{d}{2}$ ,  $E_y = D e^{-\gamma x}$   
 $x < \frac{d}{2}$ ,  $E_y = C e^{+\gamma x}$

$E_y = A \cos \alpha x$  in film,  $B = 0$ .

$E_y = C e^{+\gamma x}$  [ - for -ve  $\alpha$ , values ] in cover,  
 $= D e^{-\gamma x}$  [ - for +ve  $\alpha$ , values ]



Boundary conditions:  $E_y$  and  $H_z$  are continuous.

(i)  $(E_y)_{\text{film}} = (E_y)_{\text{cover}}$  at  $x = \frac{d}{2}$  and  $x = (-\frac{d}{2})$  (ii)

(ii)  $\left(\frac{dE_y}{dx}\right)_{\text{film}} = \left(\frac{dE_y}{dx}\right)_{\text{cover}}$  at  $x = d/2$  and  $x = (-d/2)$  (iii) (iv)

at  $x = +d/2$ .

$(E_y)_{\text{film}} = A \cos\left(\alpha \frac{d}{2}\right)$  - [sub. for  $x$ ]  
 $(E_y)_{\text{cover}} = D e^{-\gamma(d/2)}$

using B.C (i) we have.

$A \cos\left(\alpha \frac{d}{2}\right) = D e^{-\gamma \frac{d}{2}}$  — (40)

2nd B.C condition.

$\left(\frac{dE_y}{dx}\right)_{\text{film}} = -A \alpha \sin \alpha x$

$\left(\frac{dE_y}{dx}\right)_{\text{cover}} = -D \gamma e^{-\gamma \frac{d}{2}}$  — (41)



using B.C (ii) we have.

$$-A \alpha \sin\left(\frac{\alpha d}{2}\right) = -D \gamma e^{-\gamma \frac{d}{2}} \quad \text{--- (41)}$$

Dividing (41) by (40).

$$\tan\left(\frac{\alpha d}{2}\right) = \left(\frac{\gamma}{\alpha}\right) \quad \text{--- (42)}$$

$$\text{at } x = (-d/2)$$

$$(E_y)_{\text{film}} = A \cos(\alpha x).$$

$$(E_y)_{\text{cover}} = C e^{+\gamma x}$$

using B.C (iii).

$$A \cos\left(\frac{\alpha d}{2}\right) = C e^{-\left(\frac{\gamma d}{2}\right)} \quad \text{--- (43)}$$

$$\left(\frac{dE_y}{dx}\right)_{\text{film}} = -A \alpha \sin \alpha x.$$

$$\left(\frac{dE}{dx}\right)_{\text{cover}} = +\gamma C e^{\gamma x}$$

using B.C (iv) we have.

$$-A \alpha \sin\left(\frac{\alpha d}{2}\right) = -C \gamma e^{-\gamma \frac{d}{2}} \quad \text{--- (44)}$$

Dividing (44) by (43)

$$\alpha \tan\left(\frac{\alpha d}{2}\right) = \gamma$$

$$\tan\left(\frac{\alpha d}{2}\right) = \left(\frac{\gamma}{\alpha}\right) \quad \text{--- (45)}$$

consider

$$\frac{\gamma^2}{\alpha^2} = \left[ \frac{\gamma^2}{\alpha^2} + 1 - 1 \right]$$

Add and subtract.

=

$$\frac{\gamma^2}{\alpha^2} = \frac{\gamma^2 + \alpha^2}{\alpha^2} - 1,$$

substitute for  $\gamma^2, \alpha^2$

$$\frac{\gamma^2}{\alpha^2} = \left[ \frac{\beta^2 - k_0^2 n_2^2 + k_0^2 n_1^2 - \beta^2}{\alpha^2} - 1 \right]^{1/2} \quad \text{--- 46}$$

$$\frac{\gamma^2}{\alpha^2} = \left[ k_0^2 \left( \frac{n_1^2 - n_2^2}{\alpha^2} \right) \right]^{1/2} \quad \text{multiply and divide both sides by } \left(\frac{d}{2}\right)^2,$$

$$\frac{\gamma^2}{\alpha^2} = \frac{k_0^2 (n_1^2 - n_2^2) - \alpha^2}{\alpha^2}$$

$$\gamma^2 \left(\frac{d}{2}\right)^2 = \left(\frac{d}{2}\right)^2 k_0^2 (n_1^2 - n_2^2) - \left(\frac{d}{2}\right)^2 \alpha^2$$

$$\gamma \frac{d}{2} = \sqrt{\frac{v^2}{4} - \xi^2} \quad \text{--- (47)}$$

where  $v = k_0 d (n_1^2 - n_2^2)^{1/2}$  --- (48)  
 $\xi = \alpha \frac{d}{2} = (k_0^2 n_2^2 - \beta^2)^{1/2} \frac{d}{2}$  --- (49)

$v$  is dimensionless wave guide parameter.

equation (45) can be rewritten as

$$\xi \tan \xi = \left[ \frac{v^2}{4} - \xi^2 \right]^{1/2} \quad \text{--- (50)}$$

variation of  $\xi \tan \xi$  as a function of  $\xi$  is shown below.

The point of intersection of the solid and dotted curves with the quadrant of a circle of radius  $v_0 = v/2$  determine the propagation constants of the guide.

TE<sub>0</sub>, TE<sub>1</sub>, TE<sub>2</sub>.

